

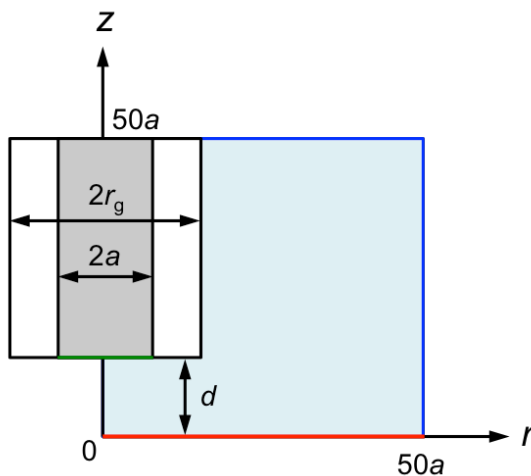
**This model was developed in the following paper.**

Chen, R.; Najarian, A. M.; Kurapati, N.; Balla, R. J.; Oleinick, A.; Svir, I.; Amatore, C.; McCreery, R. L.; Amemiya, S. "Self-inhibitory electron transfer of the Co(III)/Co(II)-complex redox couple at pristine carbon electrode." *Anal. Chem.* **2018**, *90*, 11115.

**This model is also applicable to the system discussed in the following paper.**

Chen, R.; Balla, R. J.; Li, Z. T.; Liu, H. T.; Amemiya, S. "Origin of asymmetry of paired nanogap voltammograms based on scanning electrochemical microscopy: Contamination not adsorption." *Anal. Chem.* **2016**, *88*, 8323.

**SECM Model.** Here we define a theoretical model to quantitatively describe SECM-based nanogap voltammograms of adsorption-coupled electron transfer (ET) in feedback and SG/TC modes. We consider an SECM configuration in the cylindrical coordinates (Figure 1) to define the following diffusion problem.



**Figure 1.** Scheme of the SECM configuration with a glass-insulated Pt tip ( $RG = r_g/a$ ) positioned over a macroscopic substrate. The red boundary represents the substrate surface. The green boundary represents the tip surface. Black boundaries are insulating or a symmetry axis. Blue boundaries represent the bulk solution.

A model for SECM-based nanogap voltammetry is based on the adsorption of A, that proceeds its oxidation to B, as given by



Diffusion equations for species, i (= A or B), is given in the cylindrical coordinates (Figure 1) to yield

$$\frac{\partial c_i}{\partial t} = D_i \left[ \frac{\partial^2 c_i}{\partial r^2} + \frac{1}{r} \frac{\partial c_i}{\partial r} + \frac{\partial^2 c_i}{\partial z^2} \right] \quad (3)$$

where  $D_i$  is the diffusion coefficient of species i (= A or B). The rate of the electron-transfer (ET) reaction,  $v_{\text{et}}$ , is given by the Butler–Volmer model as

$$v_{\text{et}} = k_{\text{red}} c_B - k_{\text{ox}} c_A \quad (4)$$

with

$$k_{\text{red}} = k_0 \exp \left[ -\alpha_{\text{ET}} F (E - E^{0'}) / RT \right] \quad (5)$$

$$k_{\text{ox}} = k_0 \exp \left[ (1 - \alpha_{\text{ET}}) F (E - E^{0'}) / RT \right] \quad (6)$$

where  $k_{\text{red}}$  and  $k_{\text{ox}}$  are oxidation and reduction rate constants,  $k_0$  is the heterogeneous standard ET rate constant,  $c_A$  and  $c_B$  represents the concentrations of non-adsorbed species A and B near the electrode surface, respectively,  $\alpha_{\text{ET}}$  is transfer coefficient,  $E$  is the substrate potential, and  $E^{0'}$  is the formal potential. In addition, we considered adsorption and desorption kinetics of species A on the substrate surface by using a Frumkin isotherm based on the Bragg–Williams approximation as given by

$$c_A = \frac{\theta_A}{\beta(1 - \theta_A)} \exp[-g' \theta_A] \quad (7)$$

where  $\theta_A$  is the coverage of the substrate surface with species A and is given by the ratio of the surface concentration of A,  $\Gamma_A$ , with respect to its saturated concentration,  $\Gamma_s$ ,  $\beta$  is an equilibrium parameter in

the isotherm, and  $g'$  is a parameter characterizing the magnitude of interactions among adsorbed molecules. With the Frumkin isotherm, the adsorption rate of A,  $v_{\text{ads}}$ , is given by

$$v_{\text{ads}} = k_{\text{ads}} c_{\text{A}} (\Gamma_{\text{s}} - \Gamma_{\text{A}}) - k_{\text{des}} \Gamma_{\text{A}} \quad (8)$$

with

$$k_{\text{ads}} = k_{\text{ads}}^0 \exp(\alpha_{\text{ads}} g' \theta_{\text{A}}) \quad (9)$$

$$k_{\text{des}} = k_{\text{des}}^0 \exp[-(1 - \alpha_{\text{ads}}) g' \theta_{\text{A}}] \quad (10)$$

where  $k_{\text{ads}}^0$  and  $k_{\text{des}}^0$  are standard adsorption and desorption rate constant, and  $\alpha_{\text{ads}}$  is a symmetry coefficient ( $0 < \alpha_{\text{ads}} < 1$ ) regulating the effect of  $g'$  on the adsorption activation barrier. Adsorption equilibrium is achieved at  $t = 0$  to yield eq 7 with  $\beta = k_{\text{ads}}^0 / k_{\text{des}}^0$ . Accordingly, boundary conditions at the substrate surface are given by

$$-D_{\text{A}} \left[ \frac{\partial c_{\text{A}}}{\partial z} \right]_{z=0} = v_{\text{et}} - v_{\text{ads}} \quad (11)$$

$$-D_{\text{B}} \left[ \frac{\partial c_{\text{B}}}{\partial z} \right]_{z=0} = -v_{\text{et}} \quad (12)$$

$$\left[ \frac{\partial \Gamma_{\text{A}}}{\partial t} \right] = v_{\text{ads}} \quad (13)$$

Boundary conditions at the tip depend on the operation mode, i.e.,  $c_{\text{A}} = 0$  in the feedback mode and  $c_{\text{B}} = 0$  in the SG/TC mode. In either operation mode, a current response at the tip,  $i_{\text{T}}$ , is given by

$$i_{\text{T}} = 2\pi F \int_0^a r v_{\text{et}} dr \quad (14)$$

The tip potential is given by  $E_{\text{tip}}$ .

**Dimensionless SECM Model.** Diffusion equations for species i (= A or B) are defined by using the following dimensionless parameters and solved by using a commercial finite element simulation

package, Multiphysics 5.4a (COMSOL, Burlington, MA). Specifically, diffusion equations in dimensionless forms are defined from eq S-3 for species i (= A or B) as

$$\frac{\partial C_i}{\partial \tau} = \gamma_i \left[ \frac{\partial^2 C_i}{\partial R^2} + \frac{1}{R} \frac{\partial C_i}{\partial R} + \frac{\partial^2 C_i}{\partial Z^2} \right] \quad (15)$$

with

$$C_i = c_i / c_0 \quad (16)$$

$$R = r / a \quad (17)$$

$$Z = z / a \quad (18)$$

$$\tau = D_A t / a^2 \quad (19)$$

$$\gamma_i = D_i / D_A \quad (20)$$

In addition, the potential sweep rate,  $v$ , is converted to the dimensionless form,  $\sigma$ , as

$$\sigma = a^2 v F / D_A R T \quad (21)$$

Importantly, mass transport across the tip–substrate gap maintains a quasi-steady state when  $\sigma < 1$ .

Boundary conditions at the substrate surface (eqs 11–13) are given by using dimensionless rates,  $V_{\text{et}}^{\text{SECM}}$

and  $V_{\text{ads}}^{\text{SECM}}$ , as

$$\left[ \frac{\partial C_A}{\partial Z} \right]_{Z=0} = V_{\text{et}}^{\text{SECM}} - V_{\text{ads}}^{\text{SECM}} \quad (22)$$

$$\left[ \frac{\partial C_B}{\partial Z} \right]_{Z=0} = - \frac{V_{\text{et}}^{\text{SECM}}}{\gamma_i} \quad (23)$$

$$\left[ \frac{\partial \theta_A}{\partial \tau} \right] = \frac{V_{\text{ads}}^{\text{SECM}}}{K_{\text{SECM}}} \quad (24)$$

with

$$\theta_A = \Gamma_A / \Gamma_s \quad (25)$$

$$K_{\text{SECM}} = \Gamma_s / ac_0 \quad (26)$$

$$L = d / a \quad (27)$$

Each dimensionless rate is given as follows. The dimensionless ET rate,  $V_{\text{et}}^{\text{SECM}}$ , is given by

$$V_{\text{et}}^{\text{SECM}} = \Lambda_{\text{het}}^{\text{SECM}} \left[ (\theta_{\text{ET}})^{-\alpha_{\text{ET}}} C_B - (\theta_{\text{ET}})^{1-\alpha_{\text{ET}}} C_A \right] \quad (28)$$

with

$$\Lambda_{\text{het}}^{\text{SECM}} = k^0 a / D_A \quad (29)$$

$$\theta_{\text{ET}} = \exp \left[ \frac{F(E - E_{\text{initial}})}{RT} \right] / \exp \left[ \frac{F(E^0 - E_{\text{initial}})}{RT} \right] \quad (30)$$

where  $F(E^0 - E_{\text{initial}}) / RT$  serves as a scaling factor and the substrate potential is cycled between  $E_{\text{initial}}$

and  $E_\lambda$  as the switching potential. The adsorption rate is defined in the dimensionless form,  $V_{\text{ads}}^{\text{SECM}}$ , as

$$V_{\text{ads}}^{\text{SECM}} = \Lambda_{\text{ads}}^{\text{SECM}} (\theta_{\text{ads}})^{\alpha_{\text{ads}}} C_A (1 - \theta_A) - \Lambda_{\text{des}}^{\text{SECM}} (\theta_{\text{ads}})^{\alpha_{\text{ads}}-1} \theta_A \quad (31)$$

with

$$\Lambda_{\text{ads}}^{\text{SECM}} = k_{\text{ads}}^0 \Gamma_s a / D_A \quad (32)$$

$$\Lambda_{\text{des}}^{\text{SECM}} = k_{\text{des}}^0 \Gamma_s a / c_0 D_A \quad (33)$$

$$\theta_{\text{ads}} = \exp(g' \theta_A) \quad (34)$$

The corresponding initial condition is given by

$$\frac{\Lambda_{\text{ads}}^{\text{SECM}}}{\Lambda_{\text{des}}^{\text{SECM}}} = \frac{\theta_A}{1 - \theta_A} \exp(-g' \theta_A) \quad (35)$$

Finally, a normalized tip current response,  $I_T$ , is given by

$$I_T = \frac{i_T}{FD_A c_0 a} = \int_0^1 (2\pi R V_{et}) dR \quad (36)$$

where the integral is calculated by COMSOL.

**Table 1. Parameters Used in COMSOL and Dimensionless Models.**

Parameters		Equation
COMSOL	Dimensionless Model	
rg	$RG$	
Esw	$E_\lambda - E^0$	
Erangle	$E - E_{initial}$	
sigma	$\sigma = a^2 v F / D_A R T$	21
lamda	$\Lambda_{het}^{SECM} = k^0 a / D_A$	29
theta0	$K_{SECM} = \Gamma_s / a c_0$	26
Lamda	$\Lambda_{ads}^{SECM} / \Lambda_{des}^{SECM}$	32 and 33
gprime	$g'$	7
kappa	$\Lambda_{ads}^{SECM} = k_{ads}^0 \Gamma_s a / D_A$	32
alpha	$\alpha_{ET}$	5 and 6
beta	$\alpha_{ads}$	9 and 10
gamma	$\gamma_B = D_B / D_A$	20
Etip	$E_{tip} - E^0$	