

Noise

- **Definition: Noise is unwanted signal energy in the passband of a communications device**
- **Types**
 - **White Noise (Thermal)**
 - **Shot Noise**
 - **Due to Active Devices**
 - **Electrons Moving Across Boundaries**
 - **Impluse Noise**
 - **Crosstalk**
- **Effect is Signal Corruption**

Martin B.H. Weiss

Theoretical Basis

- **Random Signal is Added to Desired Signal**
- **The Characteristics of this Random Signal Depends on the Noise Type**
 - **Thermal Noise has a Gaussian Amplitude Distribution**
 - **Shot and Impulse Noise has a Poisson Arrival Distribution**
- **The Noise Signal has an Average Frequency Characteristic**
 - **Power Spectral Density, $P(f)$, which is the Fourier Transform of the Autocorrelation function**
 - **Noise can be filtered just like any other signal**

Martin B.H. Weiss

Thermal Noise

- Due to Random Transitions of Electrons in Materials
- Proportional to Temperature
- White Noise
 - Noise that is Not Dependent on Frequency
 - Assume Power Spectral Density is Constant

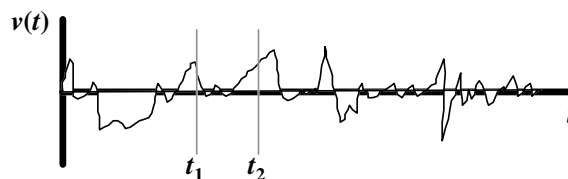
Martin B.H. Weiss

Noise and Systems - 3

University of Pittsburgh

Characterization of Thermal Noise

- Let $n(t)$ be the Noise Signal in the Time Domain
 - The Peak Voltage at Any Given Time is Random
 - Assume that the *Distribution* of Peak Voltage is Gaussian
 - Assume the Mean Voltage is Zero
 - The Noise Voltage at Time t_1 is Independent of the Noise Voltage at Time t_2
- Gaussian Distribution: $P[v(t) < x] = \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{x^2}{2\sigma^2}}$
- Graphical Representation:



Martin B.H. Weiss

Noise and Systems - 4

University of Pittsburgh

Model of Noise in the Communication Channel

- **At Any Time t_i , the Noise Voltage is Drawn From a Random Variable**
- **Thus, We Need a Different Random Variable for Each Point in Time for Which $n(t)$ has a Value**
 - **Imagine $n(t)$ has a Value for m Points in Time**
 - **We Could Imagine m Identical Noise Generators Operating Simultaneously, Continuously, and Independently**
 - **Each is Sampled at the Appropriate Time**
 - **At Time t_1 , Noise Generator 1 is Sampled**
 - **At Time t_i , Noise Generator i is Sampled**
 - **At Time t_m , Noise Generator m is Sampled**
- **Such a Collection of Random Variables is Called a *Random Process***

Martin B.H. Weiss

Ergodic Random Process

- **The Mean Value of the Random Variables are Identical**
- **The Variance of the Random Variables are Identical**
- **The Average Across Random Variables in the Ensemble (the *Ensemble Average* of the Random Process) is Identical to the Time Average of Any Random Process in the Ensemble**

Martin B.H. Weiss

Description of an Ergodic Random Process

- Mean $m = \langle n(t) \rangle = E[n(t)]$
- Variance $\sigma^2 = \langle [n(t) - \langle n(t) \rangle]^2 \rangle = \langle n^2(t) \rangle - \langle n(t) \rangle^2$
- Covariance
 - $m_{XY}(t, t+\tau) = \langle [n(t) - \langle n(t) \rangle][n(t+\tau) - \langle n(t+\tau) \rangle] \rangle$
 - or, $m_{XY}(t, t+\tau) = \langle n(t)n(t+\tau) \rangle - \langle n(t) \rangle \langle n(t+\tau) \rangle = \langle n(t)n(t+\tau) \rangle$
 - Where
 - X Refers to the Value $n(t)$ may Take on at Time t
 - Y Refers to the Value $n(t)$ may Take on at Time $t+\tau$

Martin B.H. Weiss

Description of an Ergodic Random Process

- $\langle n(t) \rangle$ is the DC Component
- $\langle n(t) \rangle^2$ is the DC Power
- σ^2 is the AC Power
- $\langle n^2(t) \rangle$ is the Total Power
- $\langle n(t)n(t+\tau) \rangle$ is the *Autocorrelation Function*, $R(\tau)$
 - This is Only a Function of τ
 - For Ergodic Processes, this is independent of t
 - In General, $R_n(\tau) = \langle n(t)n(t+\tau) \rangle = \int_{-\infty}^{\infty} n(t)n(t+\tau) dt$
 - Note That $R(0) = \langle n^2(t) \rangle = \text{Total Power}$

Martin B.H. Weiss

Power Spectral Density of Noise

- The Power Spectral Density of Noise, $P_n(f) = F\{R(\tau)\}$ (Watts/Hz)
- If the Noise is White
 - It is Uniform Across all Frequencies
 - That is, $P(f) = \frac{N_0}{2}$
 - Thus, $R(\tau) = F^{-1}\{P_n(f)\}$
 - Or, $R(\tau) = \frac{N_0}{2} \delta(\tau)$
 - Where the Function $\delta(\tau) = \begin{cases} 1 & \tau = 0 \\ 0 & \tau \neq 0 \end{cases}$
 - White Noise is Completely Uncorrelated with Itself for Any Time Delay

Martin B.H. Weiss

Filtering Noise

- Noise Behaves Like a Signal
- Therefore, $N_{out}(\omega) = |H(\omega)|N_{in}(\omega)$
- Assume a Low Pass Filter
 - $H(\omega) = \frac{1}{1 + j\omega RC}$
 - $N_{in}(\omega) = N/2$
 - $N_{out}(\omega) = \frac{N}{2} \frac{1}{1 + (\omega RC)^2}$
- In the Time Domain,
 - $R(\tau) = F^{-1}\{P_n(f)\}$
 - $R_{out}(\tau) = \frac{N}{4RC} e^{-\frac{|\tau|}{RC}}$
 - Recall That $R(0) = \text{Total Power} = \frac{N}{4RC}$
 - Note that Output Noise is No Longer Uncorrelated

Martin B.H. Weiss

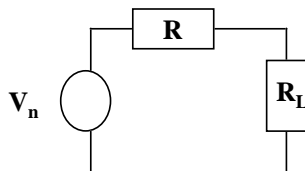
Characterization of Thermal Noise

- $P(f) = kT$
 - $P(f)$ = Power Spectral Density (Watts/Hz)
 - T = Temperature of the Conductor (in °K = 273 + °C)
 - k = Boltzman's constant = $1.38 \cdot 10^{-23}$ joule/°K
 - Example
 - Noise Power at Room Temperature (290°K)
 - $P(f) = 1.38 \cdot 10^{-23} \cdot 290 = 4 \cdot 10^{-21}$ W/Hz
- In a Particular Bandwidth B
 - The Noise Power $N = P(f) B = kTB$
 - N is in Watts

Martin B.H. Weiss

Characterization of Thermal Noise

- The Existence of Power Presupposes
 - A Generator
 - A Circuit
 - A Load
- Circuit Diagram



Martin B.H. Weiss

Characterization of Thermal Noise

- **If the “Source” Impedance is Matched to the “Load” Impedance for Maximum Power Transfer**
 - **In General, $P = V_s^2/4R_s$**
 - **Let $R_s = R$ (i.e., the Resistor Under Investigation)**
 - **Let $P = kTB$, and $V_s^2 = V_n^2$**
 - $V_n^2/R=kTB$
 - So $V_n^2 = 4RkTB$, by Substitution
 - **Also, $V_n^2 /B = 4kTR$ is the Voltage Spectral Density**
- **Generalization**
 - **This Applies to Imperfect Conductors as Well**
 - **Conductors Have Resistance**

Martin B.H. Weiss

Thermal Noise Example

- **Given**
 - $R = 10\text{K}\Omega$
 - $T = 290^\circ\text{K}$
 - $B = 1\text{MHz}$
- $V_n^2 = 4(4*10^{-21})(10^4)(10^6) = 16*10^{-11}$

Martin B.H. Weiss

Series Resistance

- **Procedure**
 - **Sum the Resistances**
 - **Sum the Noise Powers**
- **Thus,**
 - **For Each Resistor, $V_n^2 = 4RkTB$**
 - **The Total Noise is $V_n^2 = V_{n1}^2 + V_{n2}^2 + \dots$**
 - **Or, $V_n^2 = 4(R_1 + R_2 + \dots) kTB$**
- **A Similar Argument Holds for Parallel Circuits**
 - **Rely on Noise Current Instead of Noise Voltage**
 - **Use Conductances Instead of Resistances**

Martin B.H. Weiss

Reactance

- **Ideally, Reactance Does not Dissipate Heat**
- **Hence, No Noise Contribution**
- **Noise Bandwidth is Affected**

Martin B.H. Weiss

Noise Bandwidth

- **In General,**
 - $S_{n0} = |H(\omega)|^2 kT$
 - $B_{eff} = (\pi/2)(B_{3dB})$
- **This is Why Bandpass Filters are Often Included in the Front End of Communications Systems**

Martin B.H. Weiss

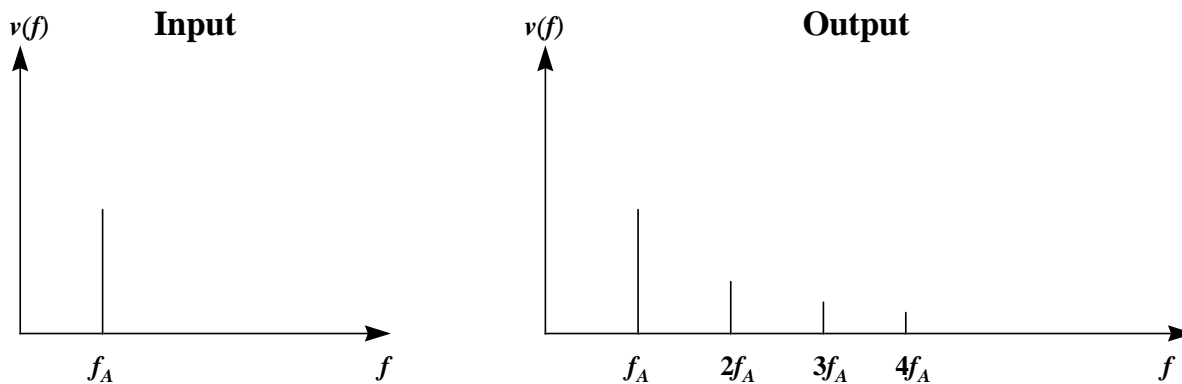
Correlated Noise

- **Result of System Non-Linearities**
- **Harmonic Distortion**
- **Intermodulation Distortion**

Martin B.H. Weiss

Harmonic Distortion

- Result of Non-Linearities
- Occurs When the Result of a A Single Input Frequency Passed Through a System Contains the Fundamental and Its Harmonics
- %Total Harmonic Distortion = $(V_{higher})/(V_{fundamental}) * 100$



Martin B.H. Weiss

Intermodulation Noise

- Product of *Two or More* Signals are Passed Through a Non-Linear System
- Common Test is *Second Order IM Distortion*
 - % IMD = $(\text{RMS of Second-Order Cross Products}) / (\text{Total RMS Amplitude of Input Frequencies}) * 100$
- Test
 - Use Four Frequencies
 - "A" Band: f_{a1} and f_{a2}
 - "B" Band: f_{b1} and f_{b2}
 - Second Order Cross Products (2A-B)
 - $(2f_{a1} - f_{b1})$
 - $(2f_{a1} - f_{b2})$
 - $(2f_{a2} - f_{b1})$
 - $(2f_{a2} - f_{b2})$
 - $(f_{a1} + f_{a2}) - f_{b1}$
 - $(f_{a1} + f_{a2}) - f_{b2}$

Martin B.H. Weiss

Noise and Amplifiers

- **General**
 - **Amplifiers Amplify Noise as well as Signal**
 - **Amplifiers Add Noise to the Signal**
- **Signal to Noise Ratio**
 - **Definitions**
 - **Voltage Ratio: $S/N = V_S^2/V_N^2$**
 - **Power Ratio: $S/N = P_S/P_N$**
 - **Common Form: $SNR = 10 \log (S/N)$**
- **Common Mode Rejection**
 - **Applies to Differential Amplifiers**
 - **Differential Amplifiers Amplify the *Difference* Between the Inputs**
 - **The Elements of the Signal that the Inputs Have in Common Should Not Be Amplified**

Martin B.H. Weiss

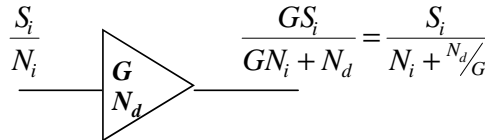
Noise Figure

- **Qualitative**
 - **Measure of the Amount of Noise Added by a System**
 - **May be Frequency Dependent**
- **Analytical Definition**
 - **Ratio of S/N at Input to S/N at Output**
 - **Noise Factor: $F = \frac{(S/N)_i}{(S/N)_o}$**
 - **Noise Figure (NF)**
 - **Noise Ratio with S/N in Decibels ($SNR_{dB} = 10 \log_{10} (S/N)$)**
 - **Thus, $SNR_{dB}(i) = SNR_{dB}(o) - NF$**

Martin B.H. Weiss

Noise Figure

- $NF \geq 0$
 - Perfect Systems Add No Noise
 - Imperfect Systems Add Noise (i.e., the SNR Decreases)
 - Analog Systems Cannot Remove Noise Due to its Random Nature
- More Specifically,
 - Gain, $G = S_o/S_i$
 - $NR = F = (N_o/N_i)(S_i/S_o) = N_o/GN_i$
 - Or $N_o = FGN_i$
 - But $N_i = kTB$, so
 - $N_o = FGkTB$



Martin B.H. Weiss

Amplifiers in Cascade

- Given a Series of Amplifiers, a_1, a_2, a_3, \dots
- With Gains G_1, G_2, G_3, \dots
- And With Noise Ratios F_1, F_2, F_3, \dots
- Then the Noise Ratio for the Series is Given by Friiss's Formula

$$F = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} + \dots$$

Martin B.H. Weiss

Noise Temperature

- **General**
 - **Another Way of Measuring Noise**
 - **Since Noise is Associated with Temperature,**
 - Its Level Can be Represented as an Equivalent Temperature
 - *i.e.*, the System Seems to be Operating Hotter Than It Is
 - **Used Frequently in Microwave Systems with Receiver Input Noise**
- **Analytical Representation**
 - Let $kT_e B = (F - 1)kT_0 B$
 - Or, $T_e = (F - 1)T_0$

Martin B.H. Weiss

Implications for Communications Systems

- **In Analog Systems,**
 - **The Repeaters Have a Noise Ratio > 1**
 - **A Repeatered Network Consists of Amplifiers in Cascade**
 - This Implies that Noise Multiplies
 - This Limits the Length of Transmission Systems
 - **Thus, in Addition to Amplifying the Signal and the Noise, they add Noise**
- **In Digital Systems, the Regenerative Repeaters Do Not Add Noise**
 - **That is, $F = 1$**
 - **Thus, Noise Does not Accumulate**
 - **In Addition, The Repeaters Can Repeat Only Signal**

Martin B.H. Weiss

Sample Noise Calculation

- **Problem**

- **Three Telephone Circuits in Series Have SNR = 44dB**
- **A Fourth Circuit is Added with SNR = 34dB**
- **What is the Overall SNR?**

- **Solution**

- **Recall that $\text{SNR}_{\text{dB}} = 10 \log_{10}[P_s/P_n]$**
- **The Signal Remains Constant Across All Circuits**
- **Thus, $\text{SNR}_{\text{dB}} = 10 \log_{10}\left(\frac{P_s}{P_{n_1} + P_{n_2} + P_{n_3} + P_{n_4}}\right)$**
- **We Can Compute the Noise Power for Each Circuit:**
 - $\frac{P_s}{P_n} = 10^{\frac{\text{SNR}_{\text{dB}}}{10}}$
 - **Thus, For the First Three Circuits, $\frac{P_s}{P_n} = 10^{\frac{44}{10}} \cong 25 \times 10^3$**
 - **For the Last Circuit, $\frac{P_s}{P_n} = 10^{\frac{34}{10}} \cong 2.5 \times 10^3$**
- **Combining,**

$$\text{SNR}_{\text{dB}} = 10 \log_{10}\left(\frac{P_s}{3P_{n_a} + P_{n_b}}\right) = 10 \log_{10}\left(\frac{P_s}{P_s\left[\frac{3}{25 \times 10^3} + \frac{1}{2.5 \times 10^3}\right]}\right) = 33 \text{dB}$$

Martin B.H. Weiss